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TEMPERATURE FIELD IN A HALFSPACE WITH A PARALLELEPIPED-SHAPED HEAT-RELEASING INCLUSION

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A study is made of the stationary temperature field in a half-space containing a foreign heat-releasing inclusion of parallelepiped shape of small dimensions.

In the operation of metalloceramic bodies of radio-electronic apparatus a need accises for studying temperature fields for bodies with foreign inclusions of small dimensions.

In this connection we consider an isotropic halfspace containing, at a distance z from its boundary surface, a foreign inclusion of parallelepiped shape and volume $V_0 = 8$ hbd in whose vicinity uniformly distributed internal heat sources of strength q_0 are operative. We refer the body in question to a rectangular cartesian coordinate system. We place the coordinate origin at the center of the inclusion. On the boundary surface z = -d-x a convective heat exchange is specified with external mean temperature t_c .

For the determination of the stationary temperature field we have the heat conduction equation [1]

$$\frac{\partial}{\partial x} \left[\lambda(x, y, z) \frac{\partial \Theta}{\partial x} \right] + \frac{\partial}{\partial y} \left[\lambda(x, y, z) \frac{\partial \Theta}{\partial y} \right] + \frac{\partial}{\partial z} \left[\lambda(x, y, z) \frac{\partial \Theta}{\partial z} \right] = -Q(x, y, z),$$
(1)

where

$$\lambda(x, y, z) = \lambda_1 + (\lambda_0 - \lambda_1) N(x, h) N(y, b) N(z, d);$$

$$Q(x, y, z) = q_0 N(x, h) N(y, b) N(z, d);$$

$$\Theta = t - t_c; N(x, h) = S(x + h) - S(x - h).$$
(2)

The boundary conditions may be written in the form

$$\lambda_{1} \frac{\partial \Theta}{\partial z} = \alpha_{z} \Theta \quad \text{for } z = -d - l, \ \Theta = 0 \quad \text{for } z \to \infty,$$

$$\Theta = 0, \ \frac{\partial \Theta}{\partial x} = 0 \quad \text{for } |x| \to \infty, \ \Theta = 0, \ \frac{\partial \Theta}{\partial y} = 0 \quad \text{for } |y| \to \infty.$$
(3)

We assume that the dimensions of the foreign inclusion are small in comparison with the distance from the coupling boundary to the boundary surface. We introduce the addiced thermal conductivity $\Lambda_0 = \lambda_0 V_0$ of the inclusion, the adduced power $Q_0 = q_0 V_0$ of the heat sources acting in it, and in Eqs. (2) we pass to the limit, letting $h \rightarrow 0$, $b \rightarrow 0$, $d \rightarrow 0$,

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maintaining Λ_0 and Q_0 constant, and using the well-known [2] limit $\lim_{h \to 0} \frac{N(x, h)}{2h} = \delta(x)$. As a result we have

$$\lambda(x, y, z) = \lambda_1 + \Lambda_0 \delta(x, y, z), \tag{4}$$

$$Q(x, y, z) = Q_0 \delta(x, y, z).$$
(5)

Although the local non-homogeneity described by the relation (4) containing the Dirac delta-function is formally concentrated at the origin, it is, in fact, characterized by finite dimensions associated with the volume V_0 . Thus the finite dimensions of the inclusion are effectively accounted for by relation (4) (see [3]).

Substituting expressions (4) and (5) into Eq. (1), we obtain the eqaution

$$\Delta\Theta + \frac{\Lambda_0}{\lambda_1} \left[\frac{\partial\Theta(x, 0, 0)}{\partial x} \Big|_{x=0}^* \delta'(x) \,\delta(y, z) + \frac{\partial\Theta(0, y, 0)}{\partial y} \Big|_{y=0}^* \delta'(y) \delta(x, z) + \frac{\partial\Theta(0, 0, z)}{\partial z} \Big|_{z=0}^* \delta'(z) \,\delta(x, y) \right] = -\frac{Q_0}{\lambda_1} \,\delta(x, y, z), \tag{6}$$

where

$$\frac{\partial \Theta(x, 0, 0)}{\partial x}\Big|_{x=0}^{*} = \frac{1}{2} \left[\frac{\partial \Theta(x, 0, 0)}{\partial x} \Big|_{x=+0} + \frac{\partial \Theta(x, 0, 0)}{\partial x} \Big|_{x=-0} \right]$$

Applying the Fourier integral transform with respect to coordinates x and y to equation (6) and conditions (2), we arrive at the following boundary value problem:

$$\frac{d^2\Theta}{dz^2} - \gamma^2 \overline{\Theta} = -P_1 \delta(z) - P_2 \delta'(z), \qquad (7)$$

$$\lambda_1 \frac{d\bar{\Theta}}{dz} = \alpha_z \bar{\Theta} \text{ for } z = -d - l, \ \bar{\Theta} = 0 \text{ for } z \to \infty,$$
(8)

where

$$\overline{\Theta} = \frac{1}{2\pi} \int_{-\infty}^{\infty} \exp i\alpha x dx \int_{-\infty}^{\infty} \Theta \exp i\beta y dy; \quad \gamma^2 = \alpha^2 + \beta^2;$$

$$P_1 = \frac{Q_0}{2\pi\lambda_1}; \quad P_2 = \frac{\Lambda_0}{2\pi\lambda_1} \frac{\partial\Theta(0, 0, z)}{\partial z} \Big|_{z=0}^*.$$

Here we have taken into account that $\frac{\partial \Theta(x, 0, 0)}{\partial x}\Big|_{x=0}^* = \frac{\partial \Theta(0, y, 0)}{\partial y}\Big|_{y=0}^* = 0.$

The solution of Eq. (7), subject to conditions (8), has the form

$$\overline{\Theta} = \frac{1}{2} \left\{ \frac{P_1}{\gamma} \left[F_1(z) - F_2(z+d_1) \right] - P_2 \left[F_1(z) \operatorname{sign} z + F_2(z+d_1) \right] \right\},$$
(9)

where

$$F_1(z) = \exp\left(-\gamma |z|\right); \ F_2(z) = \frac{\alpha_z - \lambda_1 \gamma}{\alpha_z + \lambda_1 \gamma} \exp\left(-\gamma z\right); \ d_1 = 2 \left(d+l\right)$$

Performing the inverse transform on Eq. (9) and using the reference data from [4, 5], we arrive at an expression for the dimensionless temperature

$$T = \frac{\lambda_1 l}{Q_0} \Theta = \frac{1}{4\pi} \left[\varphi^{-\frac{1}{2}}(X, Y, Z) + \varphi^{-\frac{1}{2}}(X, Y, Z+D) - \right]$$

- Bi $\psi(X, Y, Z+D) + \frac{1}{2} P_2 \left[Z \varphi^{-\frac{3}{2}}(X, Y, Z) - (Z+D) \varphi^{-\frac{3}{2}}(X, Y, Z+D) + Bi \psi_1(X, Y, Z+D) \right],$ (10)

where

$$X = \frac{x}{l}; Y = \frac{y}{l}; Z = \frac{z}{l}; D = \frac{d_1}{l}; \varphi(X, Y, Z) = X^2 + Y^2 + Z^2;$$



Fig. 1. Dependence of dimensionless temperature T on: (a) dimensionless coordinate X for Bi = 1, Z = 0.02; (b) dimensionless coordinate Z for Bi = 1, X = 0.02; (c) dimensionless coordinate Z for X = 0.02.

$$\begin{split} \psi(X, Y, Z) &= 2 \exp \operatorname{Bi} Z \int_{Z}^{\infty} \exp\left(-\operatorname{Bi} Z\right) \varphi^{-\frac{1}{2}}(X, Y, Z) \, dZ; \\ \psi_1(X, Y, Z) &= 2 \exp \operatorname{Bi} Z \int_{Z}^{\infty} Z \exp\left(-\operatorname{Bi} Z\right) \varphi^{-\frac{3}{2}}(X, Y, Z) \, dZ; \\ \frac{\partial \Theta(0, 0, z)}{\partial z} \Big|_{z=0}^{*} &= \left\{ \frac{1}{d^2} + \frac{1}{4(d+l)^2} + \frac{\operatorname{Bi}}{l} \left[\frac{\operatorname{Bi}}{l} \psi(0, 0, D) - \frac{1}{l+d} \right] \right\} / \left\{ l \left[4\pi + \frac{\Lambda_0}{\lambda_1} \left(\frac{1}{4(l+d)^3} - \frac{\operatorname{Bi}}{2l(d+l)^2} + \frac{\operatorname{Bi}^2}{l^3} \right) \psi_1(0, 0, D) \right] \right\}. \end{split}$$

For Bi = 0 expression (10) has the form

$$T = \frac{1}{4\pi} \left[\varphi^{-\frac{1}{2}}(X, Y, Z) \left(1 + \frac{1}{2} P_2 Z \varphi^{-1}(X, Y, Z) \right) + \varphi^{-\frac{1}{2}}(X, Y, Z + D) \left(1 - \frac{1}{2} P_2 (Z + D) \varphi^{-1}(X, Y, Z + D) \right) \right].$$
(11)
Here $\frac{\partial \Theta(0, 0, z)}{\partial z} \Big|_{z=0}^{*} = \left(\frac{1}{d^2} - \frac{1}{4(d+l)^2} \right) / \left[l \left(4\pi + \frac{\Lambda_0}{4\lambda_1 (d+l)^3} \right) \right].$

Using formulas (10) and (11) with Y = 0, calculations were made and a study was conducted of the dimensionless temperature distribution T for the following initial data:

TABLE 1. Dependence of Dimensionless Temperature T on Dimensionless Coordinate Z for X = 0.02

Z·10 ²	Bi			-7.10^{2}	Bi		
	0	1	5		0	1	5
22 18 14	0,6502 0,8498 1,2075	0,5924 0,7928 1,1514	0,5769 0,7781 1,1371	10 6 2	1,9731 4,2007 13,6778	1,9177 4,1460 13,6231	1,9038 4,1324 13,6094

basic material, ceramic BK94-1; inclusion material, molybdenum; $h/\ell = b/\ell = d/\ell = 0.02$. Numerical results illustrating the variation of the dimensionless temperature along coordinate X for Z = 0.02 and along coordinate Z for X = 0.02 are shown in Fig. 1; values of the dimensionless temperature for $-22 \le z \cdot 10^2 \le -2$ and Bi = 0; 1; 5 are given in Table 1.

It is evident from Figs. 1a and 1b that the temperature increases monotonically with decrease in the values of X and |Z| and attains its largest value in the region of operation of the heat sources (curve 1 in the case of a foreign inclusion in the halfspace; curve 2 in the case of a homogeneous halfspace). It is seen that presence of a foreign heat-releasing inclusion leads to a significant increase in the temperature. In the region $|Z| \leq 0.12$ a symmetry may be observed in the temperature field with respect to the plane Z = 0.

Figure 1c illustrates the dependence of temperature T on coordinate Z for various values of the Biot number. It is evident that with an increase in heat emission the temperature diminishes.

NOTATION

T(x, y, z), temperature field; $\lambda(x, y, z)$, thermal conductivity coefficient of nonhomogeneous body; λ_1 , λ_0 , thermal conductivity coefficients of basic material and of the inclusion; α_z , coefficient of heat transfer from the surface $z = -\ell - d$; S(ζ); symmetric unit function; $\Delta = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2}$, Laplace operator; $\delta(\zeta)$, Dirac delta function; Bi = $(\alpha_2 \ell)/\lambda_1$, Biot number.

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